

Estimation of Solder Ball Collapse Height in Semiconductor Packaging using Theoretical and Solid Modeling Techniques

ABSTRACT

Semiconductor packages using solder balls as interconnect to the printed circuit board (PCB) are very popular especially in mobile products like smart phones. Recent requirement to make the package much thinner is very challenging. The solder ball collapse height after the solder ball is reflowed on the package substrate metal pad would need to be tightly controlled and aligned with the required height to meet the target overall package thickness. Another challenge is that the package has to be developed in a short period of time. In this study, theoretical and solid modeling techniques were developed to estimate the solder ball collapse height and compared with actual evaluation results. With these, the solder ball collapse height could be quickly estimated to make the package design and development faster avoiding several trial evaluations on different combinations of solder ball size, substrate pad solder mask opening diameter and solder mask thickness. Based on the estimation results, using these techniques showed good agreement with actual solder ball height measurements and have now been successfully used in coming up with final package designs in a fast and cost-effective way.

Keywords: solder ball collapse height; semiconductor package; ball grid array, solid modeling

1. INTRODUCTION

Ball grid array package (BGA) is commonly used for devices in mobile applications. It is a substrate-based package that has solder balls for connecting to the printed circuit board (PCB) or flexible board in a surface mount technology (SMT) process. Fig. 1 shows a BGA package used for sensors in smart phones.

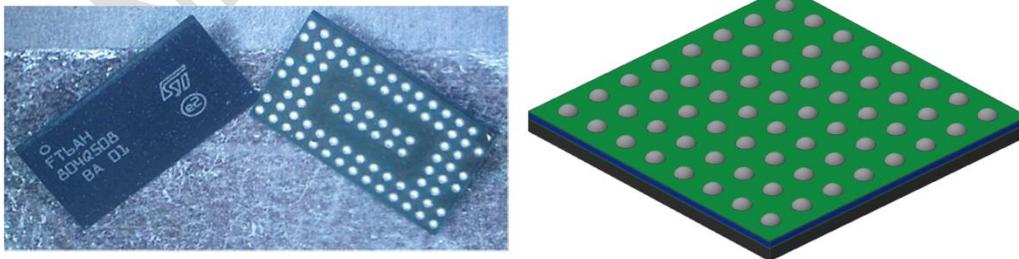


Fig. 1. BGA package showing the solder balls.

The solder balls in BGA packages are attached to the substrate by a pin-transfer process in which flux is used from a dipping tray and the solder balls are then placed into the deposits and the whole assembly is reflowed [1]. After reflow, the solder ball or solder sphere would

collapse as it attaches to the substrate metal pad. The reflowed solder ball is commonly called solder bump. The final solder ball height after reflow is the focus of this study. Control of the package thickness needs to be tighter when the package gets thinner for applications with very limited space in the thickness direction. As shown in Fig. 2, the overall package thickness A of a BGA package is composed of the solder ball collapse height A_1 , substrate thickness A_2 and epoxy mold cap thickness A_4 . To get the target overall package thickness A , the solder ball collapse height A_1 needs to be identified. However, this parameter A_1 is dependent on the solder ball size to be used, the solder mask opening diameter and the solder mask thickness. For finer solder ball pitch, the solder mask opening size needs to be reduced as well.

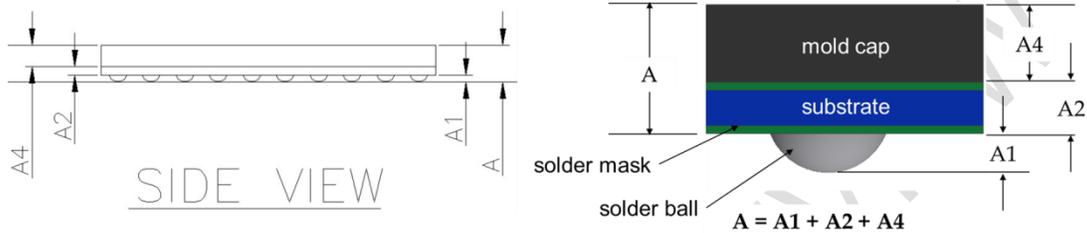


Fig. 2. Package thickness.

Therefore, correctly predicting the solder ball collapse height is very important in meeting the required overall package thickness. Most studies [2-7] used Surface Evolver software to predict the shapes of full array BGA solder joints with different solder volumes. This software is very helpful especially for resulting solder joints with complex shapes. As discussed in one previous study [3], Surface Evolver allows 3-D problems to be examined by discretizing an initial surface into a set of inter-connected triangular facets and then iterating this initial surface toward a minimal energy configuration by conjugate gradient methods. It is basically an energy-based method that considers surface tension of the material, gravitational effects, and internal/external pressures. This Surface Evolver software is robust and quite powerful but it is not very convenient to use for semiconductor package designers whose tools are mainly solid modeling or CAD (computer aided-design) software like SolidWorks or Autodesk Inventor. It is also observed that solder ball shape after reflow of a BGA package is not complex and could be estimated by some simple approximation. This study presents simplified techniques developed for predicting solder ball collapse height that would be very useful for package designers to use and make the design and development much faster.

2. SOLDER BALL COLLAPSE HEIGHT ESTIMATION

When the solder ball is reflowed after being placed on the substrate metal pad, the shape is basically transformed from a sphere to a hemispherical cap and a cylindrical volume within the solder mask thickness, t . This happens when the solder melts during reflow and fills the circular metal pad area as shown in Fig. 3. In this study, a solder mask defined pad (SMD) pad is considered. For SMD substrate pad, the pad size is defined by the solder mask opening diameter. The solder mask opening exposes the metal pad on which the solder ball would be reflowed.

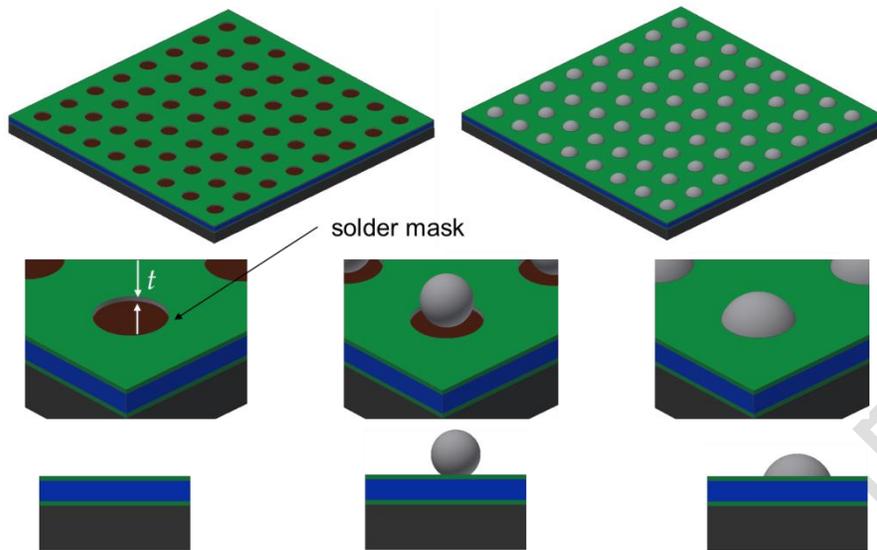


Fig. 3. Solder ball transformation before and after reflow.

2.1 Theoretical Technique

Since the solder ball is just transformed to a different shape during ball attach and reflow, conservation of mass is considered. For solder material, the volume of the original solder ball (sphere) would be equal to the volume of the reflowed solder ball with a certain collapse height. This is illustrated in Fig. 4. In the study, the volume of the reflowed solder ball was simplified as the sum of volume of the hemispherical cap, V_s , and the cylindrical volume, V_c .

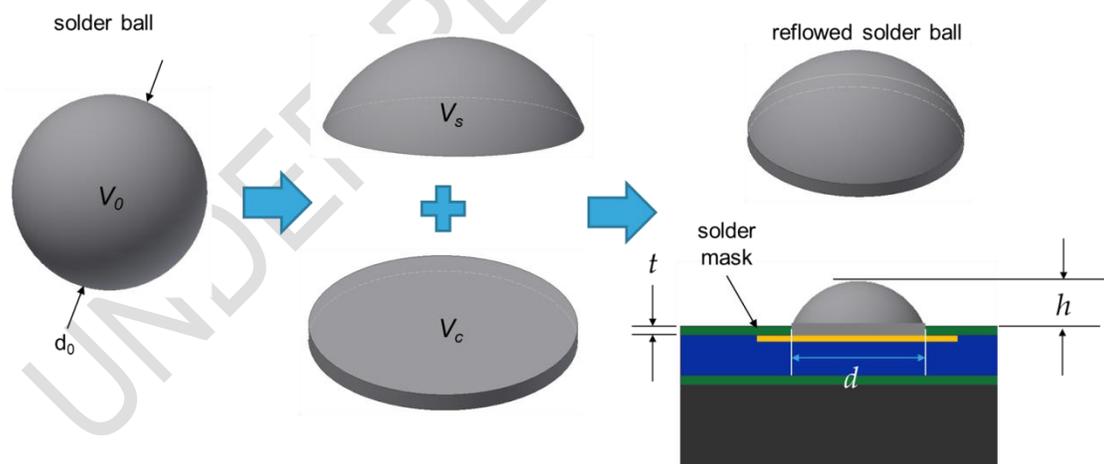


Fig. 4. Original solder ball to a reflowed solder ball.

The original solder volume, V_0 , is given by the formula below:

$$V_0 = \frac{4}{3} \pi \left(\frac{d_0}{2} \right)^3$$

Fig. 5 shows details of a hemispherical cap from which the volume estimation of one portion of the reflowed solder was derived. This spherical cap volume, V_s , could be calculated using the formula:

$$V_s = \frac{\pi h}{6}(3a^2 + h^2)$$

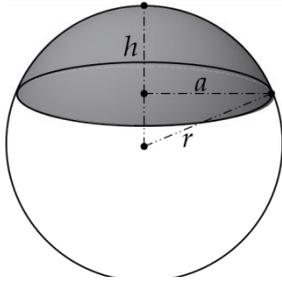


Fig. 5. Hemispherical cap.

The other portion of the reflowed solder volume is shown in Fig. 6 and this cylindrical volume, V_c , could be calculated with the formula shown below:

$$V_c = \frac{\pi d^2}{4}(t)$$

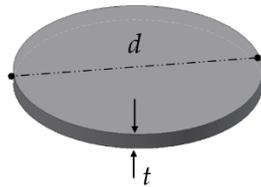


Fig. 6. Cylindrical volume.

The volume of the original solder ball is dependent only on the solder ball size or diameter, d_0 . On the other hand, the volume of the reflowed solder ball is dependent on the solder mask thickness t , solder mask opening diameter d , and solder ball collapse height h . The value of a in Fig. 5 is equal to half of the solder mask opening diameter d .

Using the solver macro of Microsoft Excel and selecting the “GRG Nonlinear” solving method, the value of the reflowed solder ball collapse height h was determined by minimizing the difference between the original solder ball volume and the reflowed solder ball, where the difference is given by the equation below:

$$\text{Volume Difference} = V_0 - (V_c + V_s)$$

The solution method is basically an iterative process to find the value of the solder ball collapse height given the other known parameters. In situations where the target solder ball collapse height h is given, then the same process is also applicable to find the correct solder ball size to be used.

2.2 Solid Modeling Technique

Semiconductor package designers are usually using solid modeling or CAD (computer-aided design) software like SolidWorks and Autodesk Inventor to create 3-D package designs. CAD software enables the designer to see the designed part as if it were real. The solid model can be rotated or viewed in different directions and helps the designer identify any problem with the design that needs to be corrected before actual manufacturing. Solid models created could also be directly used for any package stress or deformation analysis to make sure the package structure is robust.

CAD software has the capability of determining the volume of any solid model created even how complex the shape is. When package designs are created in 3-D model using solid modeling software, the best approach is to create the whole package as an assembly. It means that the reflowed or collapsed solder ball would be created as a separate solid model part. Other components like substrate, mold encapsulation would also be created as separate parts. Without knowing any formula for solving the volume of a given solid, package designers would be able to get the volume of each solid model in the whole package assembly design. Modeling the reflowed solder ball as a separate part would make the evaluation of the reflowed solder ball volume easy. In this study, Autodesk Inventor was used to create the solid model parts.

3. RESULTS AND DISCUSSION

For the specific BGA package considered, the requirement from customer was to maintain the solder mask opening diameter at 300 μm and solder mask thickness at 20 μm . Different solder ball sizes were considered. Using the theoretical technique described earlier, the results are summarized in Table 1. It shows that using 220 μm solder ball would produce 102 μm solder ball collapse height.

Table 1. Summary of Solder Ball Collapse Height Calculation Results

Ball Diameter (μm)	Solder Mask Opening Diameter (μm)	Solder Mask Thickness (μm)	Solder Ball Collapse Height (μm)
170	300	20	32
180	300	20	45
200	300	20	73
220	300	20	102
240	300	20	131

With solid modeling technique, the volume of the solid model part was easily determined as shown in Fig. 7 for the solder ball before reflow. The solid model shown (sphere) is having a diameter equal to 220 μm .

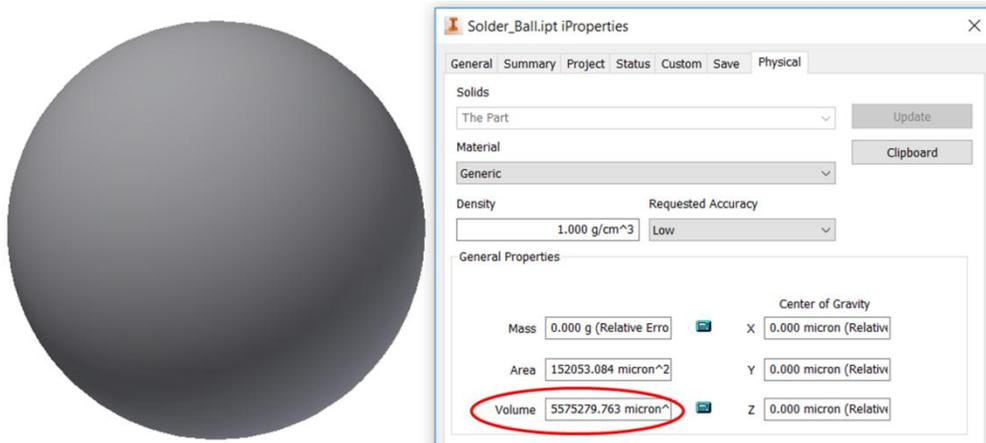


Fig. 7. Volume of the original solder ball determined using solid modeling software.

Fig. 8 shows the solid model of the cylindrical volume of the reflowed solder ball. It has 300 μm diameter, which is also the same as the solder mask opening. The thickness is 20 μm and this is the same as the solder mask thickness.

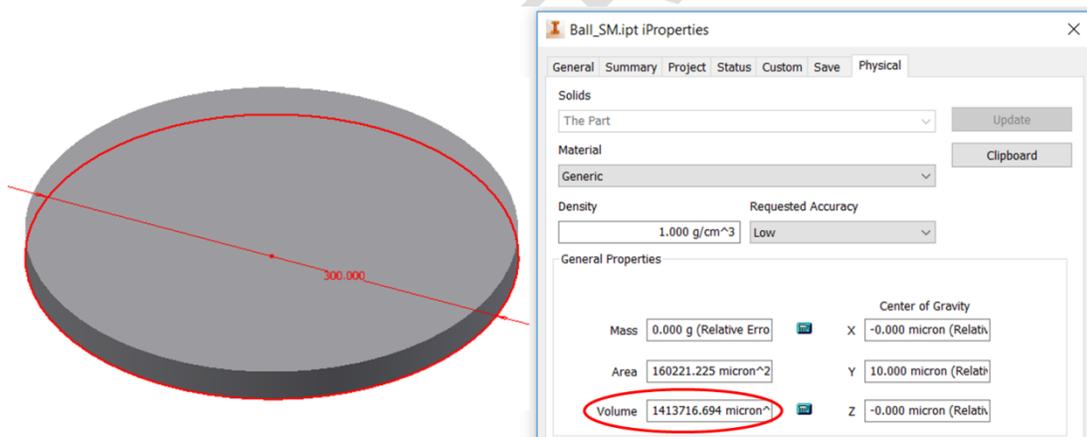


Fig. 8. Volume of the reflowed solder ball within the solder mask thickness.

After evaluating the volume of the original solder ball and the cylindrical volume of the portion of the reflowed solder ball, the hemispherical cap solid model was adjusted so that the volume of the original solder ball would be equal to the volume of the reflowed solder ball. Fig. 9 shows that the final solder ball collapse height determined from the solid model is 102 μm . Results show that theoretical calculation yields the same result as the solid modeling approach.

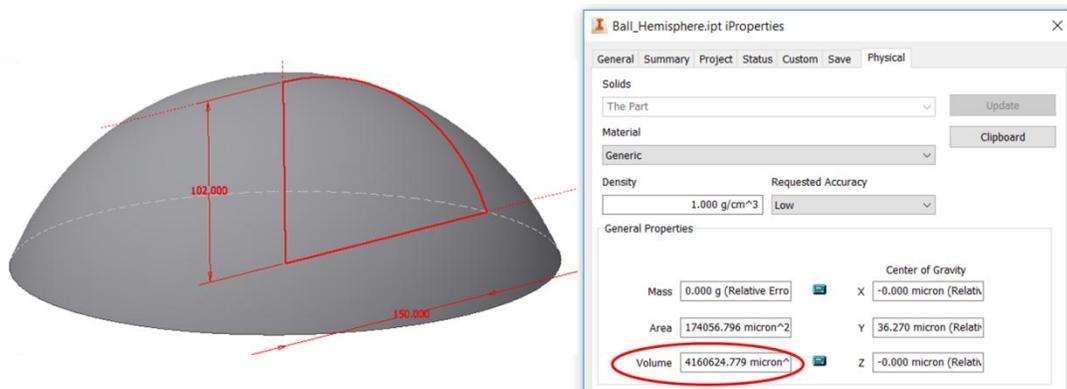


Fig. 9. Volume of the hemispherical cap portion of the reflowed solder ball.

Actual solder ball collapse height measurements were analyzed using Minitab, a statistical analysis software. The actual data distribution is shown in Fig. 10. As we can see, the mean value of the solder ball collapse height is 100 μm . This is very close to the estimation obtained by the theoretical and solid modeling techniques.

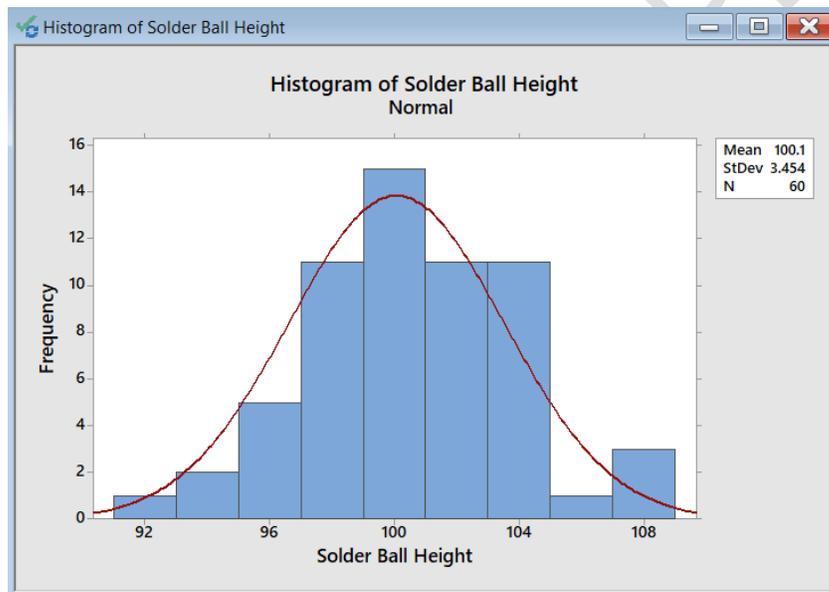


Fig. 10. Actual solder ball collapse height measurements.

Fig. 11 shows the actual image of the reflowed solder. The final solder shape is very similar to the solid model simplified approximation created using CAD software.

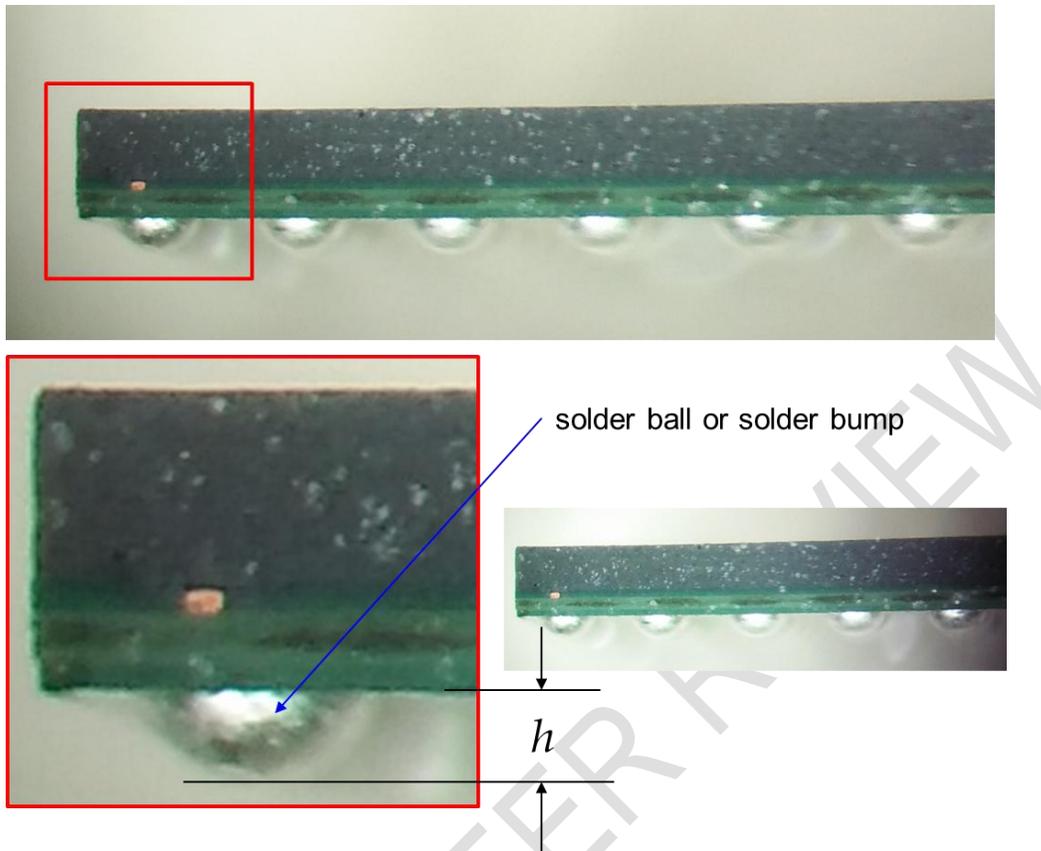


Fig. 11. Package side view showing the solder ball collapse height measured in this study.

4. CONCLUSION

Based on the actual solder ball collapse height measurements, the theoretical and solid modeling techniques explored here were able to give quite accurate results for the specific BGA package analyzed. Solder ball collapse height estimations were very close to the actual measurements. Simple use of Microsoft Excel and solid modeling software readily available to package designers would be able to provide quick estimation of the solder ball collapse height and is very useful in assessing design options to meet the target overall package thickness for semiconductor BGA packages. The estimation techniques presented would also be very useful for exploring different BGA package design options like reduction in solder mask opening size especially for BGAs requiring finer solder ball pitch, reduction in solder mask thickness, and other package design adjustments based on available solder ball size.

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Authors have declared that no competing interests exist. The products used for this research are commonly and predominantly use products in our area of research and country. There is absolutely no conflict of interest between the

authors and producers of the products because we do not intend to use these products as an avenue for any litigation but for the advancement of knowledge. Also, the research was not funded by the producing company rather it was funded by personal efforts of the authors.

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